

Rock rheology – time dependence of dilation and stress around a tunnel

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- Poynting-Thomson: not one of the many
- Unloading – rod
- Unloading – circular tunnel
- Conclusions

Rock rheology – the Poynting-Thomson model

$$\rho \dot{\mathbf{v}} + \operatorname{div} \mathbf{F} = \rho \mathbf{f} \quad \text{balance of momentum}$$

$$f(\mathbf{D}, \boldsymbol{\xi}) = \hat{f}(\mathbf{D}) + \boldsymbol{\xi} : \boldsymbol{\xi} \quad \text{Helmholtz free energy}$$

$$T\sigma_s = \left(\mathbf{F} + \rho \mathbf{D} \frac{\partial f}{\partial \mathbf{D}} \right) : \dot{\mathbf{D}} \mathbf{D}^{-1} - \boldsymbol{\xi} : \dot{\boldsymbol{\xi}} \geq 0.$$


Universal – independent of microstructure

$$\mathbf{F}^E = \mathbf{T} + \sigma_0 \mathbf{I} = 2G\mathbf{E} + 3K\varepsilon_0 \mathbf{I}$$

Ideal elastic

$$\mathbf{F} = \mathbf{T} + \sigma_0 \mathbf{I} \quad (\text{tr } \mathbf{T} = 0)$$

Small deformation

$$\mathbf{D} = \mathbf{E} + \varepsilon_0 \mathbf{I} \quad (\text{tr } \mathbf{E} = 0)$$

Isotropic

$$\left(\mathbf{T} + \sigma_0 \mathbf{I} - (2G\mathbf{E} + 3K\varepsilon_0 \mathbf{I}) \right) : \dot{\mathbf{D}} - \boldsymbol{\xi} : \dot{\boldsymbol{\xi}} \geq 0.$$

Entropy production

$$\begin{aligned} \mathbf{T} - 2G\mathbf{E} &= L_{11} \dot{\mathbf{E}} - L_{12} \boldsymbol{\xi}, \\ \boldsymbol{\xi} &= L_{12} \dot{\mathbf{E}} - L_{22} \boldsymbol{\xi}, \\ \sigma_0 - 3K\varepsilon_0 &= L \dot{\varepsilon}_0, \end{aligned}$$

$$\mathbf{T} - 2G\mathbf{E} = L_{11}\dot{\mathbf{E}} - L_{12}\dot{\boldsymbol{\xi}},$$

$$\dot{\boldsymbol{\xi}} = L_{12}\dot{\mathbf{E}} - L_{22}\dot{\boldsymbol{\xi}},$$

$$\sigma_o - 3K\varepsilon_o = L\dot{\varepsilon}_o,$$

$$L > 0, L_{11} > 0, L_{22} > 0,$$

$$L_{11}L_{22} - L_{12}^2 > 0$$

$$\tau = L_{22}^{-1}, \quad \tau_d = L_{11}L_{22}^{-1},$$

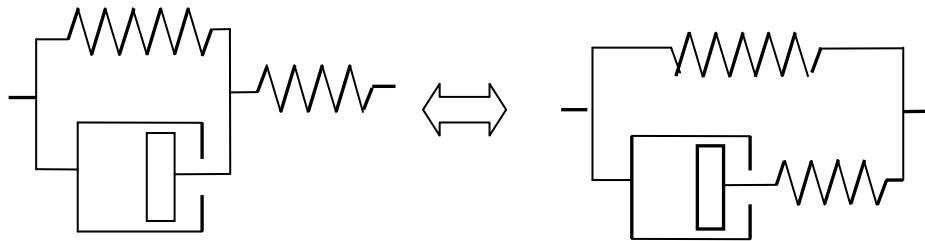
$$2\eta = L_{11} - L_{12}^2 L_{22}^{-1} + 2GL_{22}^{-1},$$

$$\tau > 0, \quad \tau_d > 0,$$

$$\eta > G\tau,$$

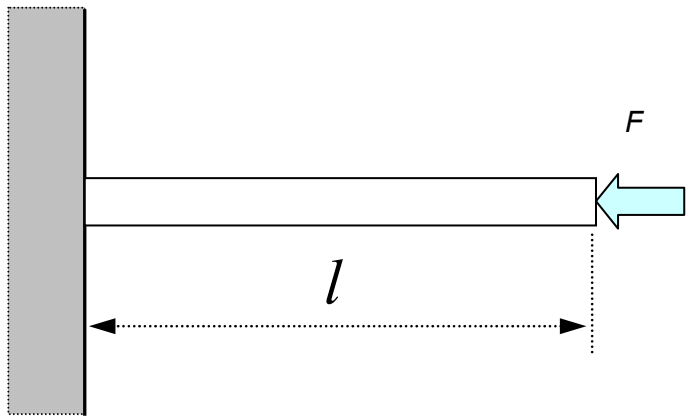
$$\mathbf{T} + \tau \dot{\mathbf{T}} = 2G\mathbf{E} + 2\eta \dot{\mathbf{E}} + \tau_d \ddot{\mathbf{E}},$$

$$\sigma_o = 3K\varepsilon_o + L\dot{\varepsilon}_o.$$



Poynting-Thomson =
Hooke+Kelvin-Voigt

Opening of 1D tunnel – released rod



$$\mathbf{T} + \tau \dot{\mathbf{T}} = 2G\mathbf{E} + 2\eta \dot{\mathbf{E}},$$
$$\sigma_o = 3K\varepsilon_o.$$

Three stages:

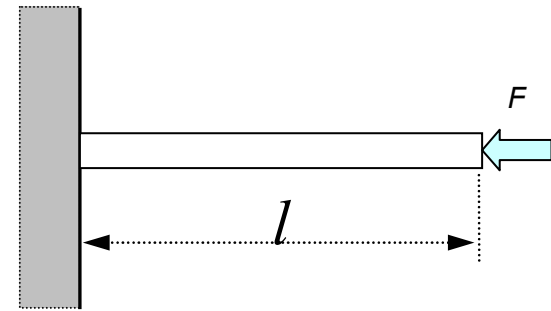
primary: equilibrium is linear elastic

Opening: new initial condition

secondary: processes after the opening

A) Released rod – primary stage

$$\begin{aligned} \mathbf{T}_A &= 2G\mathbf{E}_A, \\ \sigma_{oA} &= 3K\varepsilon_{oA}. \end{aligned}$$



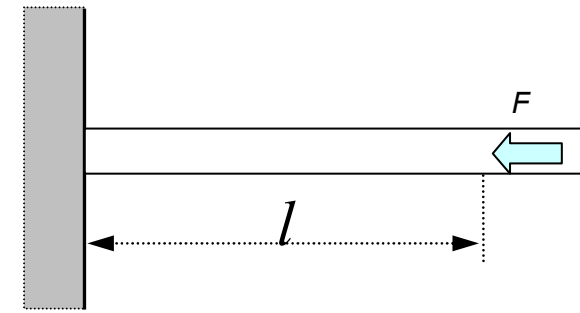
$$p = F/A$$

$$\mathbf{D}_A = \mathbf{E}_A + \varepsilon_{oA}\mathbf{I} = \begin{pmatrix} \varepsilon_x & 0 & 0 \\ 0 & \varepsilon_y & 0 \\ 0 & 0 & \varepsilon_z \end{pmatrix} = \frac{p}{3} \begin{pmatrix} \frac{1}{3K} + \frac{1}{G} & 0 & 0 \\ 0 & \frac{1}{3K} - \frac{1}{2G} & 0 \\ 0 & 0 & \frac{1}{3K} - \frac{1}{2G} \end{pmatrix}$$

Elastic equilibrium

B) Released rod – opening

$$\tau \dot{\mathbf{T}}_B = 2\eta \dot{\mathbf{E}}_B$$

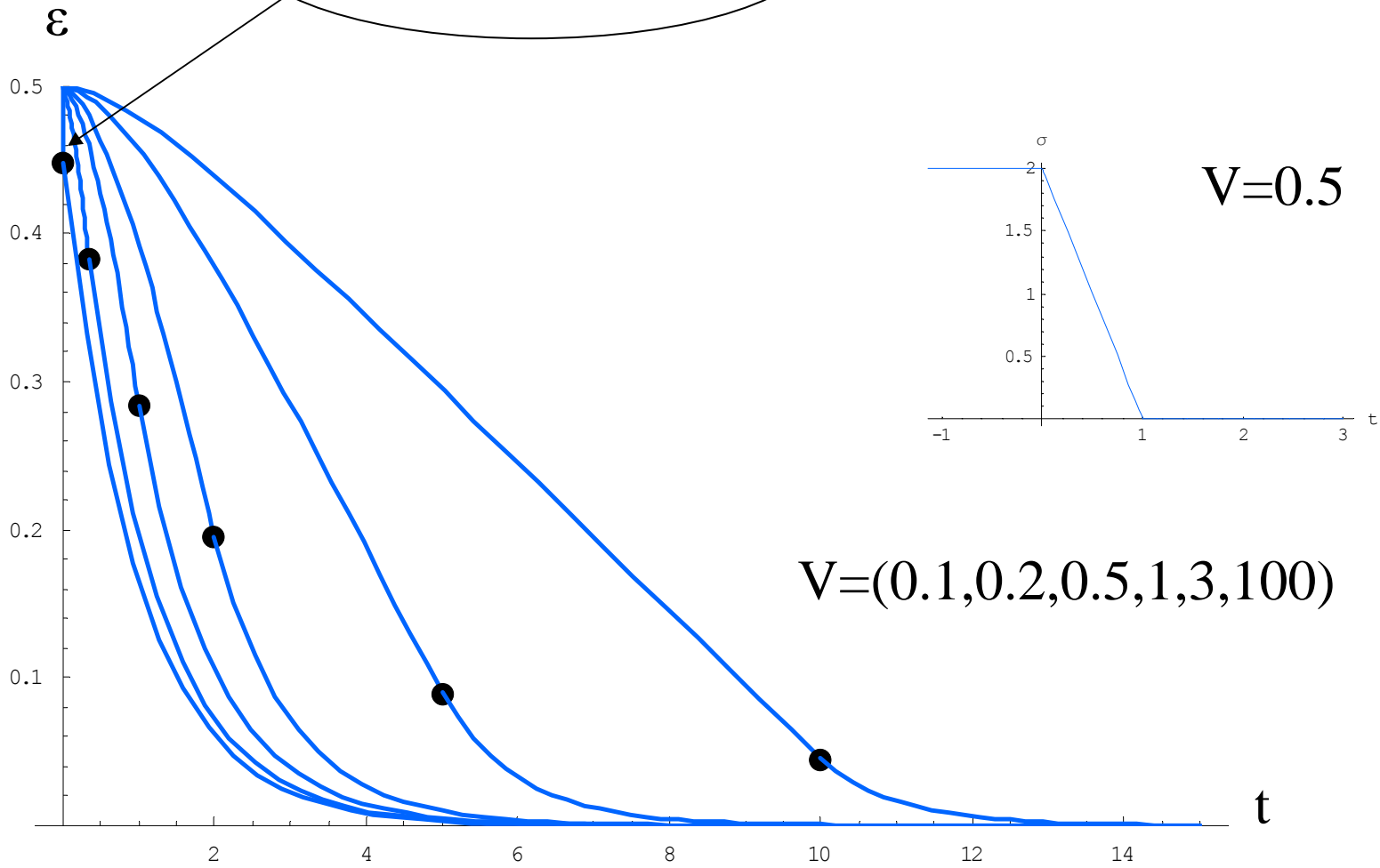
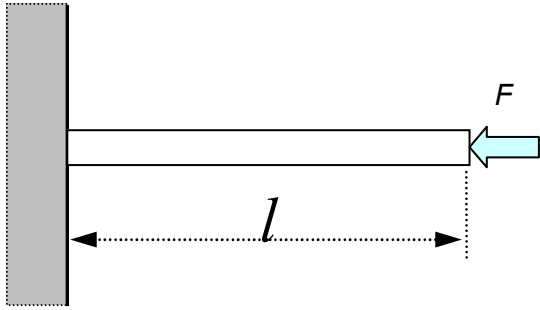


Fast, “quasielastic” $p = F/A$

Finally:

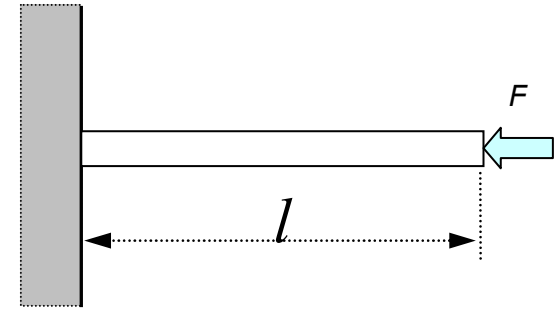
$$\mathbf{D}_B = \frac{\mathbf{T}_A}{2G} \left(1 - \frac{\tau G}{\eta} \right) = \frac{p}{6G} \left(1 - \frac{\tau G}{\eta} \right) \begin{pmatrix} 2 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{pmatrix}.$$

jump: $\Delta\varepsilon_1 = .045$



B) Released rod – secondary

$$\begin{aligned} \mathbf{T} + \tau \dot{\mathbf{T}} &= 2G\mathbf{E} + 2\eta \dot{\mathbf{E}}, \\ \sigma_o &= 3K\varepsilon_o. \end{aligned}$$



$$\mathbf{D}(t = 0) = \mathbf{D}_B \quad \text{Initial condition}$$

Finally:

$$\mathbf{D}(t) = \mathbf{D}_B e^{-\frac{G}{\eta}t} = \frac{p}{6G} \left(1 - \frac{\tau G}{\eta} \right) e^{-\frac{G}{\eta}t} \begin{pmatrix} 2 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{pmatrix}$$

Opening of a circular tunnel

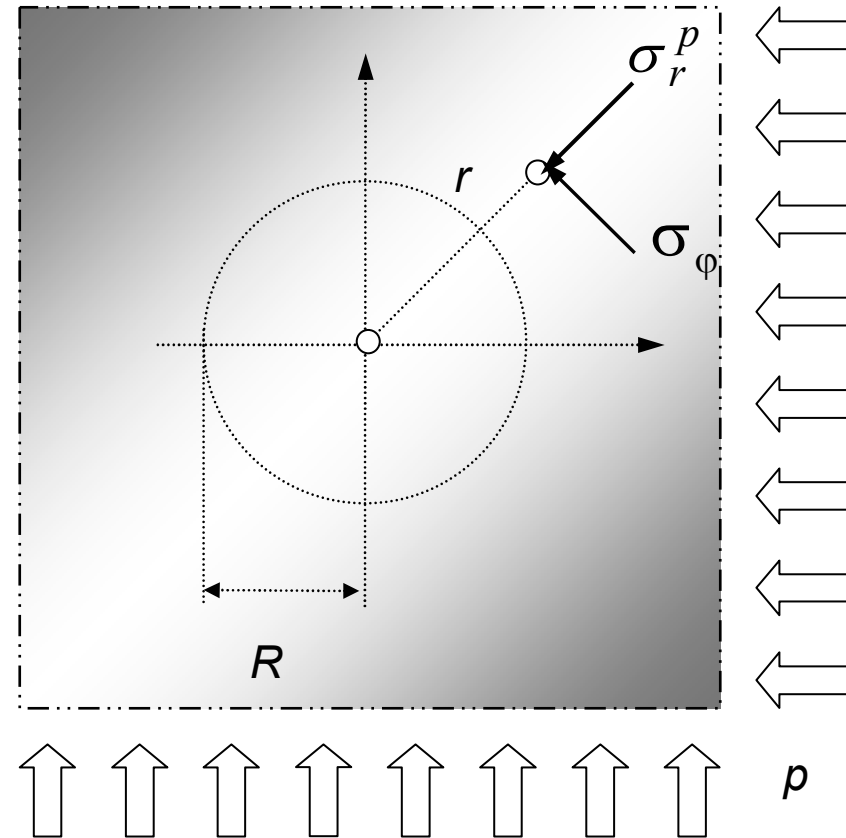
$$\mathbf{T} + \tau \dot{\mathbf{T}} = 2G\mathbf{E} + 2\eta \dot{\mathbf{E}},$$
$$\sigma_o = 3K\varepsilon_o,$$
$$\text{div}(\mathbf{T} + \sigma_o \mathbf{I}) = 0.$$

Three stages:

primary: equilibrium is
linear elastic

opening: new initial condition

secondary: processes after the opening



Cylindrical symmetry

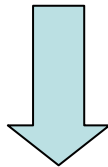
$$\frac{\partial \sigma_r}{\partial r} + \frac{\sigma_r - \sigma_\phi}{r} = 0$$

$$\tau \dot{\sigma}_r + \sigma_r = (K + 4G/3)\varepsilon_r + (K - 2G/3)\varepsilon_\phi +$$

$$(K\tau + 4\eta/3)\dot{\varepsilon}_r + (K\tau - 2\eta/3)\dot{\varepsilon}_\phi,$$

$$\tau(\dot{\sigma}_r - \dot{\sigma}_\phi) + \sigma_r - \sigma_\phi = 2G(\varepsilon_r - \varepsilon_\phi) +$$

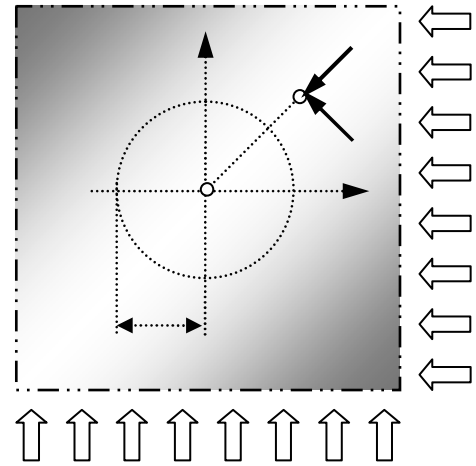
$$2\eta(\dot{\varepsilon}_r - \dot{\varepsilon}_\phi).$$



$$\left(1 + \alpha_o \frac{\partial}{\partial t}\right) \left(\frac{\partial^2 u}{\partial r^2} + \frac{1}{r} \frac{\partial u}{\partial r} - \frac{u}{r} \right) = 0$$



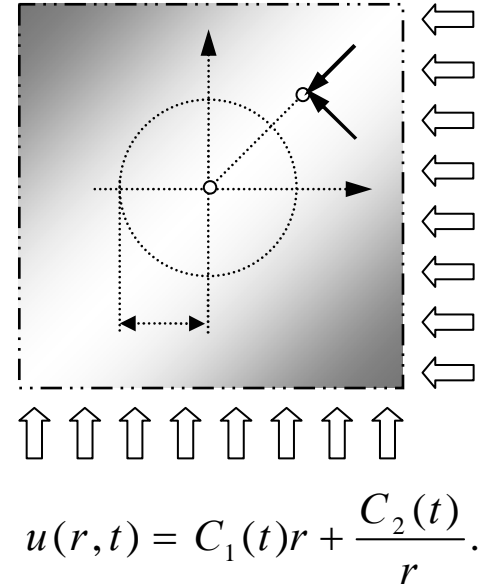
$$u(r, t) = C_1(t)r + \frac{C_2(t)}{r}.$$



Initial conditions:

$$\varepsilon_{rB} = \frac{p}{2} \left(\frac{3}{G+3K} - \frac{\tau}{\eta} \left(\frac{R}{r} \right)^2 \right) = \varepsilon_A \left(-\frac{p\tau}{2\eta} \left(\frac{R}{r} \right)^2 \right)$$

$$\varepsilon_{\phi B} = \frac{p}{2} \left(\frac{3}{G+3K} + \frac{\tau}{\eta} \left(\frac{R}{r} \right)^2 \right) = \varepsilon_A + \frac{p\tau}{2\eta} \left(\frac{R}{r} \right)^2.$$



Asymptotic condition:

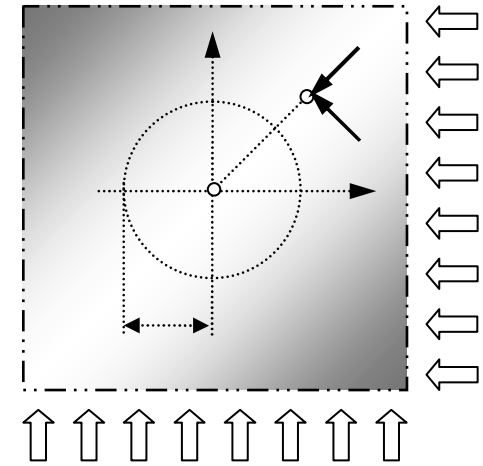
$$u(r, t = \infty) = \varepsilon_A r + \frac{p}{2G} \frac{R^2}{r},$$

$$\varepsilon_r(r, t = \infty) = \varepsilon_A - \frac{p}{2G} \left(\frac{R}{r} \right)^2, \quad \varepsilon_\phi(r, t = \infty) = \varepsilon_A + \frac{p}{2G} \left(\frac{R}{r} \right)^2,$$

$$\sigma_r(r, t = \infty) = p \left(1 - \left(\frac{R}{r} \right)^2 \right), \quad \sigma_\phi(r, t = \infty) = p \left(1 + \left(\frac{R}{r} \right)^2 \right).$$

Time dependent radial displacement:

$$u(r,t) = \varepsilon_A r + \frac{p}{2G} (1 - e^{-\frac{t}{\alpha}}) \frac{R^2}{r} + \frac{p\tau}{2\eta} e^{-\frac{t}{\beta}} \frac{R^2}{r}.$$



$$u(r,t) = C_1(t)r + \frac{C_2(t)}{r}.$$

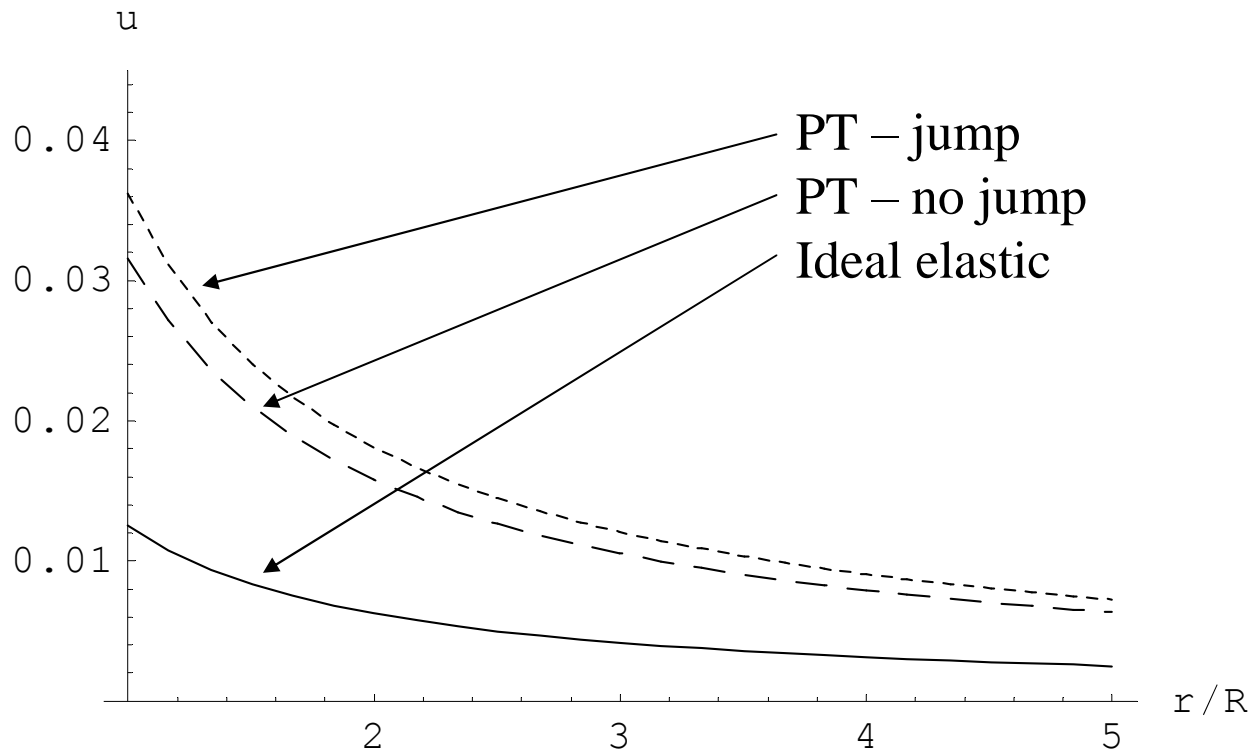
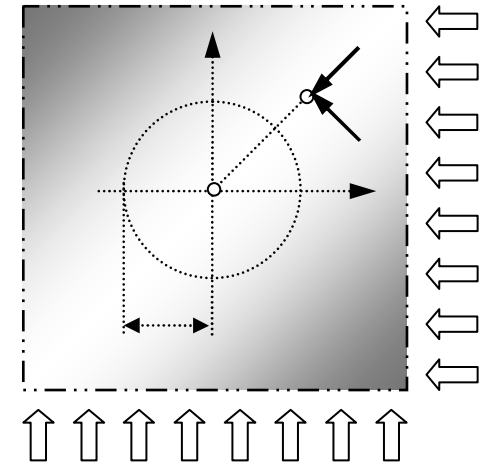
Time dependent deformation fields:

$$\varepsilon_r(r,t) = \varepsilon_A - \frac{p}{2G} (1 - e^{-\frac{t}{\alpha}}) \left(\frac{R}{r}\right)^2 - \frac{p\tau}{2\eta} e^{-\frac{t}{\beta}} \left(\frac{R}{r}\right)^2,$$

$$\varepsilon_\phi(r,t) = \varepsilon_A + \frac{p}{2G} (1 - e^{-\frac{t}{\alpha}}) \left(\frac{R}{r}\right)^2 + \frac{p\tau}{2\eta} e^{-\frac{t}{\beta}} \left(\frac{R}{r}\right)^2.$$

Radial displacement :

$$u(r,t) = \varepsilon_A r + \frac{p}{2G} (1 - e^{-\frac{t}{\alpha}}) \frac{R^2}{r} + \frac{p\tau}{2\eta} e^{-\frac{t}{\beta}} \frac{R^2}{r} .$$

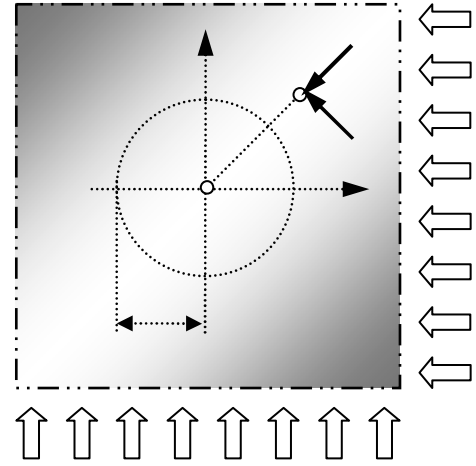


$G=10000\text{MPa}$,
 $K=30000\text{MPa}$,
 $p=1$,
 $R=1\text{m}$,
 $\eta=400000\text{MPah}$
 $t=10\text{h}$,
 $\alpha=9\text{h}$
 $\beta=11\text{h}$

Time dependent stress field:

$$\sigma_r(r, t) = p \left(1 - \left(\frac{R}{r} \right)^2 \right) + \sigma_t(r, t),$$

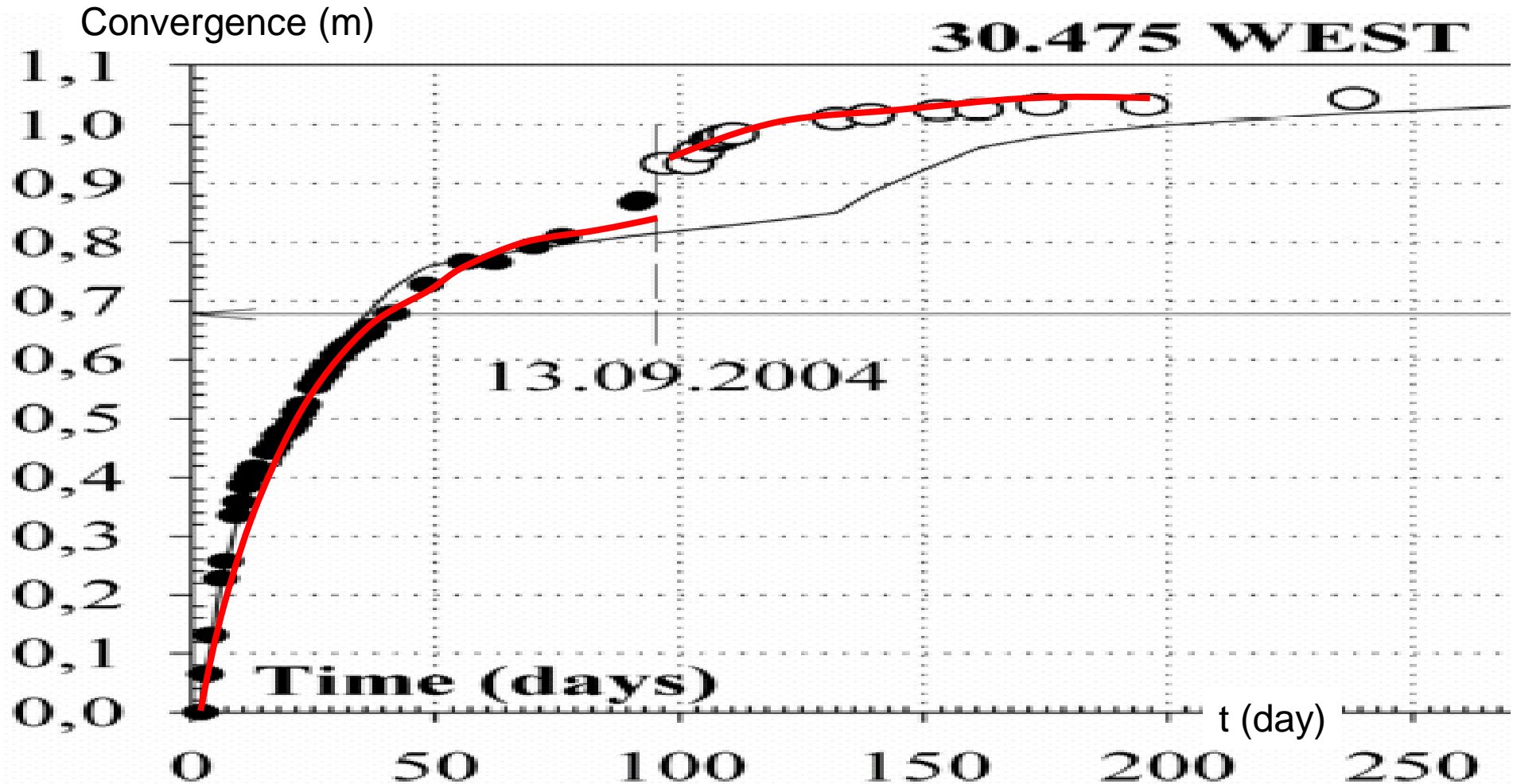
$$\sigma_\phi(r, t) = p \left(1 + \left(\frac{R}{r} \right)^2 \right) - \sigma_t(r, t),$$



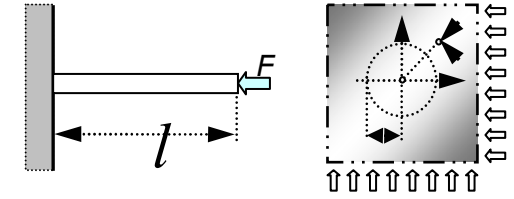
$$\sigma_r(r, t) = p \left(\frac{R}{r} \right)^2 \left(\frac{\tau(G\beta - \eta)}{\eta(\tau - \beta)} e^{-\frac{t}{\beta}} - \frac{(G\alpha - \eta)}{G(\tau - \alpha)} e^{-\frac{t}{\alpha}} + \right.$$

$$\left. (G\tau - \eta) \left(\frac{1}{G(\tau - \alpha)} - \frac{\beta}{\eta(\tau - \beta)} \right) e^{-\frac{t}{\tau}} \right).$$

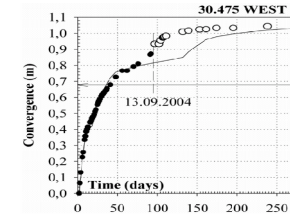
Remark to the presentation of
F. Sandrone, J.P. Dudt, V. Laiouse and F. Dexcoeudres



Conclusions



- Poynting-Thomson is not just one of them
- Separate timescales: initial jump
- Analytical solution can be generalized:
elliptical, lining, etc.
- Measurements of the material parameters
- Numerics
- mesh: gradient generalization (thermodynamics!)
- Practice:
stops and starts in tunnel excavations
swelling?



Thank you for your attention!